Phase space - some recent experiments in beam physics

Beam Adapters or Phase Space Converters Round to flat beam transformer FBT & transverse to longitudinal emittance exchange EEX

H. Edwards

Magic

to transform or produce by or as if by magic

- The Breakaway from conventional uncoupled systems (x,x'); (y, y'); (z, z')
- Round magnetized beam -> flat beam
 For σ²=<x²>=<y²>, A transformer ratio
 ε(x, x'); ε(y,y') -> Aε(σ,σ); (1/A) ε(σ',σ');
- Longitudinal <->transverse emittance exchange (EEX)

- $\varepsilon(x, x') \rightarrow \varepsilon(z, z')$ and $\varepsilon(z, z') \rightarrow \varepsilon(x, x')$

Round to Flat Beam Transform (FBT)

• Conventional RF gun wisdom- The Bz field on the cathode must be ~zero or it will contribute to beam emittance $\varepsilon_n = \frac{eB_c r_c^2}{8 m c^2}$



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A simple representation of the idea



Solenoid end field provides twist

Quad transformer with phase advance in y $\pi/2$ different from x > line at 45 deg, does not rotate

Round-to-flat beam transformation: simple-minded model



Particles are aligned diagonally; an additional 45° rotation (*skew*) for both x and y will align the particles along x or yaxis.

90 deg rotation between x and y $\begin{bmatrix} x \\ p_x \\ y \\ p_y \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} x_0 \\ p_{0x} \\ y_0 \\ p_{0y} \end{bmatrix}$ p_x $\uparrow \mathbf{y} \quad x = a\cos\theta$ (b) $y = -a\sin(\theta + 90^\circ)$ #4 #3 #1 Х #2 flat

Derbenev's more complete transformation

 $S = R_{45}^{-1} \begin{pmatrix} M & 0 \\ 0 & N \end{pmatrix} R_{45}, \text{ where } R \text{ is 45 deg rotation}, M, N 2x2 \text{ matries}$ $M = -N \cdot F, \quad F = \begin{pmatrix} 0 & \frac{1}{k_1} \\ -k_1 & 0 \end{pmatrix}, \quad k_1 = \sqrt{k^2 + \frac{{\sigma'}_0^2}{{\sigma_0}^2}}$

The betatron phase advance between M and N must be $\pi/2$ The β 's, α 's same at both ends

The resulting emittance

for
$$\varepsilon_{0} = \sigma_{0}\sigma_{0}^{'}$$
, $\sigma_{0}^{2} = \langle x_{0}^{2} \rangle = \langle y_{0}^{2} \rangle$, etc for $\sigma_{0}^{'}$
 $\varepsilon_{x} = \sqrt{\varepsilon_{0}^{2} + (k\sigma_{0}^{2})^{2}} + k\sigma_{0}^{2} = \sigma_{0}^{2} \left[\sqrt{\frac{\sigma_{0}^{'2}}{\sigma_{0}^{2}} + k^{2}} + k \right] \approx 2k\sigma_{0}^{2}$
 $\varepsilon_{y} = \sqrt{\varepsilon_{0}^{2} + (k\sigma_{0}^{2})^{2}} - k\sigma_{0}^{2} = \sigma_{0}^{2} \left[\sqrt{\frac{\sigma_{0}^{'2}}{\sigma_{0}^{2}} + k^{2}} - k \right] \approx \frac{\varepsilon_{0}^{2}}{2k\sigma_{0}^{2}} = \frac{\sigma_{0}^{'}}{2k}$
 k the matching condition $k = \frac{eB_{z,c}}{2p_{z}} = \frac{1}{\beta}$,
" \approx " for $k\sigma_{0}^{2} \gg \varepsilon_{0}$, $k \gg \frac{\sigma_{0}^{'}}{\sigma_{0}}$
 $\frac{\varepsilon_{x}}{\varepsilon_{y}} \approx \frac{(2k\sigma_{0}^{2})^{2}}{\varepsilon_{0}^{2}} = \frac{4k^{2}\sigma_{0}^{2}}{\sigma_{0}^{'2}}$, and $\varepsilon_{x}\varepsilon_{y} = \varepsilon_{0}^{2}$

canonical angular momentum $L = \gamma m r^2 \dot{\phi} + \frac{1}{2} eB_z r^2$, $\langle L \rangle = eB_c \sigma_0^2 \rightarrow 2k \sigma_0^2 p_z$

 $\left(k = \frac{eB_{z,c}}{2p_{z2}}\frac{\sigma_w^2}{\sigma_c^2} \quad \text{if beam momentum at transformer is different from that at solenoid end}\right)$



Measurement of mechanical angular momentum in a drift space

Demonstration of conservation of canonical angular momentum

as a function of magnetic field on cathode





Position and velocity snap shots at the entrance/exit of the transformer



Removal of angular momentum and generating a flat beam

	Experiment		Simulation
	90%	95%	(ASTRA)
rms_cathode(mm)	0.97		0.97
B_cathode(Gauss)	898		898
I_Quad1 (A)	-1.97		-1.98
I_Quad2 (A)	2.56		2.58
I_Quad3 (A)	-4.55		-5.08
rms_X7y (mm)	0.58±0.01	0.63±0.01	0.77
rms_X7x (mm)	$0.084{\pm}0.001$	0.095 ± 0.001	0.058
rms_X8_hslit (mm)	1.57±0.01	1.68 ± 0.01	1.50
rms_X8_vslit (mm)	0.12±0.01	0.13±0.01	0.11
Lcath (mm mrad)		24.5±0.7	
Lmech (mm mrad)		26.6±0.5	
Emit-uncorrelated (mm mrad		5.1±0.7	
$\varepsilon_+ \text{ (mm mrad)}$ 53.8±0.9			
ε_{-} (mm mrad)	0.49±0.13		
Ex (mm mrad)	<u>0.39±0.02 (0.32)</u>	<u>0.49±0.02 (0.41)</u>	<u>0.27</u>
ɛy (mm mrad)	35.2±0.5	41.0±0.5	53
εy/εx	90±5 (110+-7)	83±4 (100+-5)	196
$(\varepsilon \mathbf{x} \cdot \varepsilon \mathbf{y})^{0.5}$	3.7 (3.35)	4.5 (4.1)	3.8 mm mrad
	() camera resolution corrected		

Compare measurement with simulation

EEX

not a Derbenev idea but akin in spirit References

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Thanks to T. Koeth, A. Johnson, Y. Sun for many view graphs





EEX Thin Lens Approx (1)

Emittance exchange thin lens approximation.

Following the notation of D. Edwards (Ref $\,$), let α be the bend of each magnet in a dogleg and L₁ the distance between bends, then the dog leg matrix is given by

$$M_{dog} = \begin{pmatrix} 1 & L_1 & 0 & \alpha L_1 \\ 0 & 1 & 0 & 0 \\ 0 & \alpha L_1 & 1 & \alpha^2 L_1 \\ 0 & 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 & D/\alpha & 0 & D \\ 0 & 1 & 0 & 0 \\ 0 & D & 1 & \alpha D \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

where D is the dispersion. Let this be followed by a drift, L_2 to a thin lens deflection mode cavity. The cavity matrix is given by

$$M_{cav} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & T & 0 \\ 0 & 0 & 1 & 0 \\ T & 0 & 0 & 1 \end{pmatrix}$$

EEX Thin Lens Approx (2)

Where for exchange T= -1/D = $\frac{-1}{\alpha L_1} = \frac{\omega}{c} \frac{eV_{cav}}{E_{beam}}$ and V_{cav} is the deflection strength of the

cavity and E_{beam} is the beam energy. The total exchange

$$M_{dog}L_{2}M_{cav}L_{2}M_{dog} = \begin{pmatrix} 0 & 0 & -\frac{1}{\alpha} - \frac{L_{2}}{D} & -L_{2}\alpha \\ 0 & 0 & \frac{-1}{D} & -\alpha \\ -\alpha & -\alpha L_{2} & 0 & 0 \\ \frac{-1}{D} & \frac{-1}{\alpha} - \frac{L_{2}}{D} & 0 & 0 \end{pmatrix}$$

In our geometry D=0.33m and α = 22.5 deg.

For a finite length cavity, the (4,3) element of the M_{cav} enters and the on diagonal (coupling) blocks start to show non zero values and will dilute the 2D emittances, especially the smaller one. The finite length cavity also causes the equilibrium orbit to follow a stair case trajectory through the cavity. These effects can be compensated to some extent by suitable choices of beam and cavity parameters.

For a finite length cavity 43 element does not vanish

Measured EEX Transport Matrix



Red on-diagonal 2x2's ->0, except R43 finite length cavity The vertical plane is unaffected by the cavity status

EEX Layout & Recent Results





We determine the transverse emittances using the slit emittance technique [3]. Input x and y measurements are made using the X3-X6 diagnostic cross pair. Output x and y values are determined from the X23-X24 cross pair. Longitudinal emittance measurements are made from the minimum energy spread as measured in the spectrometer magnets and the bunch length as determined at X9 and X24. The measured emittance growth is partially explained by the present longitudinal diagnostic's inability to account for longitudinal position-energy correlation. Other possible contributions to a greater than 1:1 emittance exchange include the non-ideal emittance exchange matrix, i.e. effects of the thick lens cavity, space charge forces and potential coherent effects, such as coherent synchrotron radiation.



Longitudinal pulse shaping using EEX: transverse density to energy modulation 4



Longitudinal pulse shaping using EEX: direct measurement of temporal modulation



Some Possible Applications

- ILC damping ring- flat to round in long straights (tune shift reduction) FBT
- ILC injector with Flat εx/ εy ratio (do away with electron damping ring) FBT
- FEL emittance repartition for lower energy linac, shorter gain length FBT & EEF
- Bunch compression w/o energy chirp EEX
- Micro bunching EEX

Combinations of FBT and EEX to change emittance partition in x,y,z

Examples: Kim, Carlsten, Zholents

K. J. Kim Producing Matched e-Beams for X-Ray HG FEL

- Electron beam emittance should be matched to the radiation emittance: $\epsilon_{xn} \sim \gamma \lambda / 4\pi$
- For 1-Å with E=5 GeV, the matched emittance is $\epsilon_x^n \sim 0.1 \,\mu$ m, which is smaller by an order of magnitude than the current state-of-the-art
- In current HGFEL projects, the mismatch is dealt with by a high E (>15 GeV), high K (3.7), and high current (a few kA)
- Noting that $\Delta E/E_{slice} < 10^{-6}$, two orders of magnitudes smaller than required, the FBT and EEX can be employed to produce a matched beam



Power gain length *LG* of an x-ray FEL at 0.4 Å versus the undulator parameter *K* for (a) a beam with a normalized transverse emittance 1×10^{-6} m-r and a peak current 3.5 kA and (b) a beam with a normalized transverse emittance 1×10^{-7} m-r and a peak current 1 kA. The relative rms energy spread in both cases is 1×10^{-4} (courtesy of Z. Huang).

B. Carlsten: What We Are Thinking For New Baseline Design for MaRIE 50 keV XFEL



Zholents & Zolotorev A schematic of the bunch compressor

(manipulate longitudinal phase space with ease of a transverse phase space)

Focusing properties of individual sections



Conclusions

- The dam has broken
- The fish are free
- Magic is in
- New ideas abound
- Thanks Slava
- Thanks to: D. Edwards, R. Fliller, A. Johnson, T. Koeth, A. Lumpkin, W. Muranyi, P. Piot, J. Ruan, J. Santucci, Y.-E Sun, R. Thurman-Keup